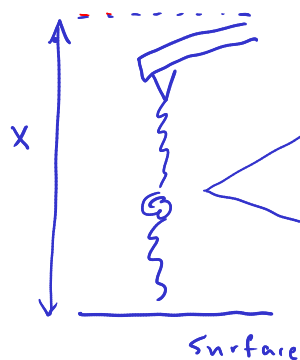
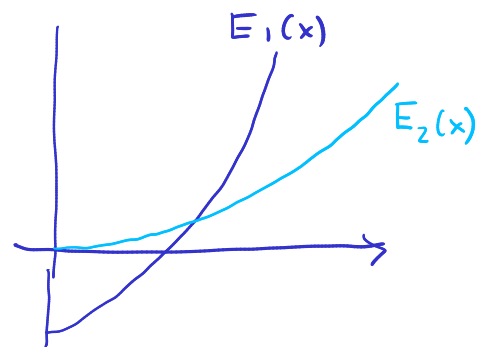


PHYS 414: 4-13-20



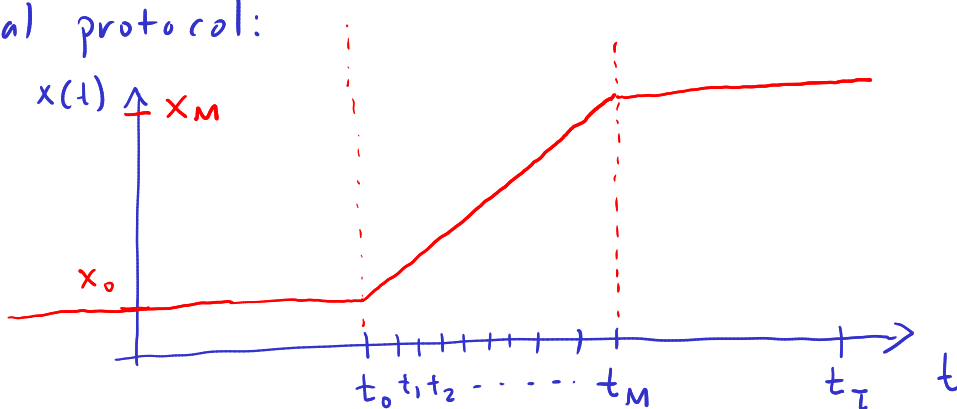
1) \odot folded $E_1(x)$
 $W_{21}(x) \downarrow$ $W_{12}(x) \uparrow$
 2) \curvearrowright unfolded $E_2(x)$

$$k_1 > k_2$$



$$\text{MR: } \frac{W_{21}(x)}{W_{12}(x)} = e^{-\beta(E_2(x) - E_1(x))}$$

Experimental protocol:

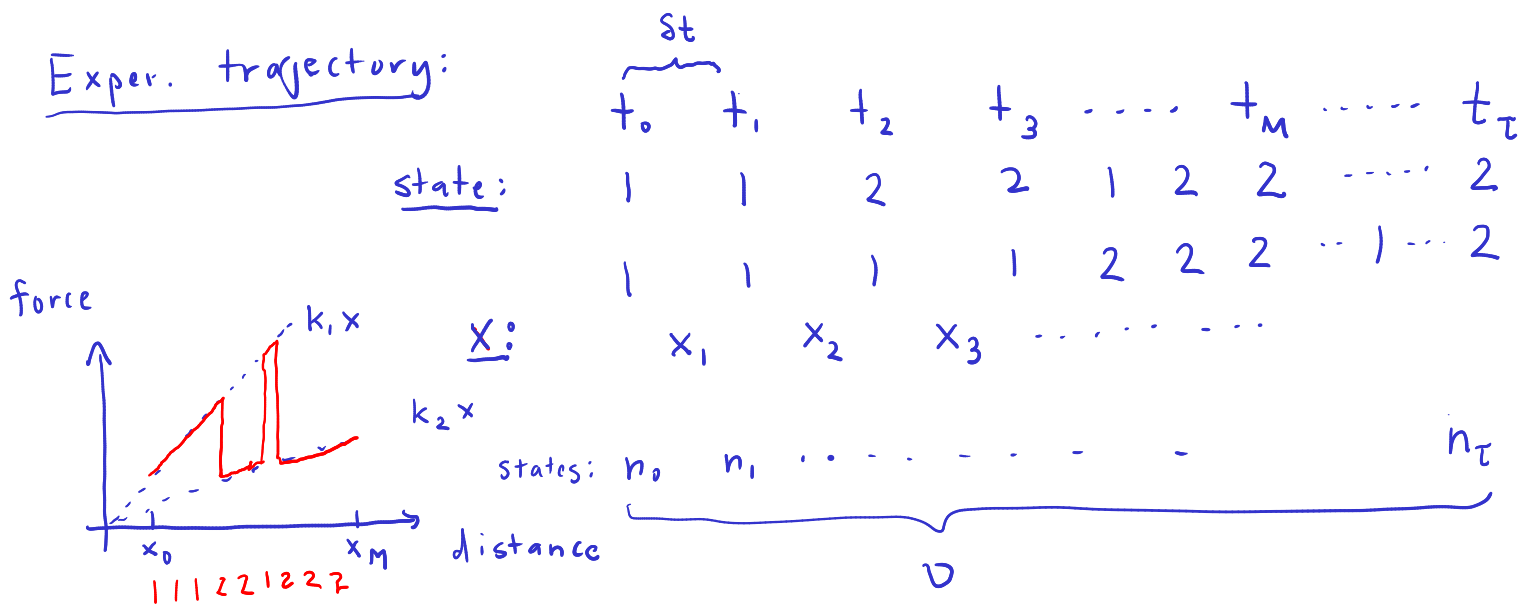


regime I:
 allow sys. to
 equilibrate at
 x_0 for a long
 time before t_0

II:
 pull the
 molecule by
 increasing
 x

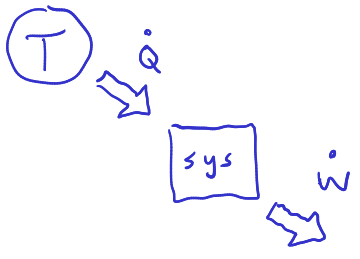
III:
 allow the sys
 to find equil.
 again at final
 separation of x_M

Exper. trajectory:



$$e^{\frac{\Delta S^i(v)}{k_B}} = \frac{\mathcal{P}(v)}{\tilde{\mathcal{P}}(\tilde{v})} \rightarrow \mathcal{P}(v) = W_{n_\tau, n_{\tau-1}}(x_\tau) \dots W_{n_1, n_0}(x_1) p_{n_0}^{eq}(x_0)$$

prob. of traj. running exper. in forw. protocol



$$\tilde{\mathcal{P}}(\tilde{v}) = W_{n_0, n_1}(x_1) \dots W_{n_{\tau-1}, n_\tau}(x_\tau) p_{n_\tau}^{eq}(x_\tau)$$

prob. of rev. traj. \tilde{v} when running exper. in backwards prot.

amount of energy (heat) donated from ext. env. in this state trans.

MR: $\frac{W_{n_{i+1}, n_i}(x_{i+1})}{W_{n_i, n_{i+1}}(x_{i+1})} = e^{-\beta (E_{n_{i+1}}(x_{i+1}) - E_{n_i}(x_{i+1}))}$

equil \Rightarrow Boltz equil: $p_{n_0}^{eq}(x_0) = \frac{e^{-\beta E_{n_0}(x_0)}}{Z(x_0)}$

$$Z(x_0) = e^{-\beta E_1(x_0)} + e^{-\beta E_2(x_0)}$$

$$p_{n_\tau}^{eq}(x_\tau) = \frac{e^{-\beta E_{n_\tau}(x_\tau)}}{Z(x_\tau)}$$

$$\frac{\mathcal{P}(v)}{\tilde{\mathcal{P}}(\tilde{v})} = e^{-\beta [(E_{n_\tau}(x_\tau) - E_{n_{\tau-1}}(x_\tau)) + \dots + (E_{n_1}(x_1) - E_{n_0}(x_0))]}$$

$\Delta Q(v)$ = total amount of heat from ext. env. in traj. v

$$\cdot e^{\beta (E_{n_\tau}(x_\tau) - E_{n_0}(x_0))} \frac{Z(x_\tau)}{Z(x_0)}$$

$\Delta E(v)$

= total energy diff. from t_0 to t_τ in traj. v

$$\Delta Q(v) = \Delta E(v) + \underbrace{\Delta W(v)}_{\text{work done by sys in traj. } v} \quad \text{1st law energy budget}$$

$$\Rightarrow \frac{P(v)}{\tilde{P}(\tilde{v})} = e^{-\beta [\Delta E(v) + \Delta W(v)]} e^{\beta \Delta E(v)} \frac{Z(x_m)}{Z(x_0)}$$

$$= e^{-\beta \Delta W(v)} \frac{Z(x_m)}{Z(x_0)}$$

$$F = \bar{E} - TS \Rightarrow \text{in equil.} \quad F^{eq} = -k_B T \ln Z$$

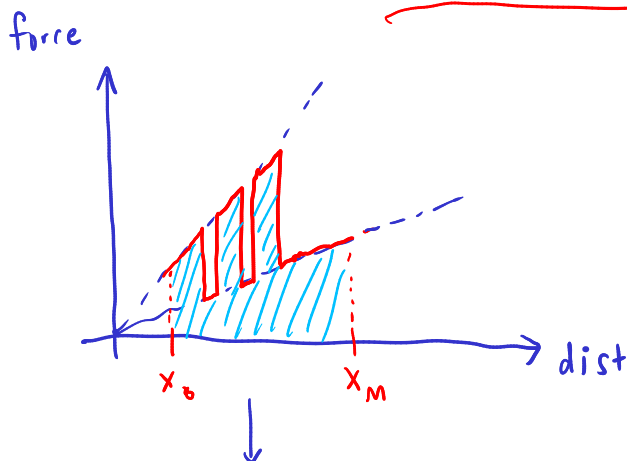
does not depend on v

$$\left. \begin{aligned} F^{eq}(x_m) &= -k_B T \ln Z(x_m) \\ F^{eq}(x_0) &= -k_B T \ln Z(x_0) \end{aligned} \right\} \begin{aligned} \Delta F \\ = F^{eq}(x_m) \\ - F^{eq}(x_0) \end{aligned}$$

$$\frac{P(v)}{\tilde{P}(\tilde{v})} = e^{-\beta [\Delta W(v) + \Delta F]} = e^{\Delta S^i(v) / k_B}$$

$$\Rightarrow \Delta S^i(v) = - \frac{(\Delta W(v) + \Delta F)}{T}$$

entropy prod. in traj.



area under curve = work done by ext. deg. of freedom (apparatus) on sys = $-\Delta W(v)$